

# Evaluation of Intersystem Interference between NavIC, GPS and Galileo

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# ABSTRACT

The paper provides an assessment of compatibility among NavIC, GPS and Galileo systems. Simulations are performed taking into account the intersystem interference between NavIC and GPS system in L5 band and NavIC and Galileo in L5 and E5a band on Indian region. Parameters considered in simulation are Space Constellation, ground cycle repeat time of satellite, EIRP etc. It is shown that the intersystem interference of Galileo caused by NavIC is slightly larger than interference of IRNSS due to Galileo. Similarly, the intersystem interference of GPS caused by NavIC is slightly larger than interference of NavIC due to GPS. Maximum interference is considered for all the cases.

#### **Keywords**

NavIC, GPS, Galileo

### **1. INTRODUCTION**

India has developed an independent Indian Regional Navigation Satellite System (IRNSS), now called NavIC (Navigation with Indian Constellation) which would provide navigational services for restricted and civil users. Its main aim is to provide reliable positioning, navigation and timing services over Indian region.

Since the frequency bands for the Global Navigation signal systems (GNSS) are already congested, the spectrum overlap of the NavIC signals and the signals of other navigation satellite systems is inevitable. Sharing the same frequency bands can benefit users as the interoperability between the NavIC and other systems. However, this also causes interference in the desired signal and result into performance degradation. Thus it is necessary to evaluate the compatibility between them. Compatibility is defined such that the interference between GNSS systems is not supposed to lie above a well-defined threshold, so that degradation of the positioning accuracy due to interference is negligible [1,2].

NavIC shares L5 band with GPS and Galileo systems which provide the opportunity of interoperability between NavIC, GPS and Galileo but also causes interference in the desired signal resulting in performance degradation. The compatibility between NavIC and GPS, as well as NavIC and Galileo are investigated in this paper. Similar analysis has been computed between Galileo and GPS [3]. Interference between these systems should not lie above a threshold so that the performance degradation is negligible. Intersystem interference between NavIC & GPS and NavIC & Galileo are computed in order to obtain worst case performance degradation on Indian region. This paper is organised as follows: Section 1 describes signal parameters and Constellation parameters of NavIC, GPS and Galileo. Section 2 provides intersystem interference analysis.

Section 3 shows simulation results of Mean received power and interference of these systems. Section 4 draws conclusion.

#### 2. OVERVIEW OF NAVIC, GPS AND GALILEO NAVIGATION SYSTEMS 2.1 Signal Parameters

# **2.1 Signal Parameters**

NavIC broadcast signal in two bands namely L5 (1176.472 MHz) band and S (2492.028 MHz) band [27]. Galileo broadcast signal in E1 band (1575.42 MHz), E5a (1176.42 MHz), E5b (1207.14 MHz) and E6 band (1278.75 MHz) [25]. GPS broadcast signal in L1 band (1575.42 MHz), L2 band (1227.6 MHz) and L5 (1176.45 MHz) as listed in Table 1 [3, 4, 5,6,7,8,9 10 & 23].

Fable	1:	Signal	Parameters

SYSTEM	SERVICE	CARRIER	MODULATION
	SERVICE	FREQUENCY(MHz)	TYPE
	E1a		
	E1b	1575.42	MBOC(6,1)
	E1c		
GALILEO	E5a	1176.42	AltBOC(15,10)
	E5b	1207.14	AltBOC(15,10)
	E6a	1079 75	BOC(10,5)
	E6b	1278.75	BPSK(5)
GPS	L1 (C/A)		BPSK(1)
	L1(P)	1575.42	BPSK(10)
	L1(M)		BOC(10,5)
	L1C		MBOC
	L2C		BPSK(1)
	L2(P)	1227.6	BPSK(10)
	L2(M)		BOC(10,5)
	L5	1176.45	BPSK(10)
NavIC	L5(SPS)	1176 472	BPSK(1)
	L5(RS)	11/0.4/2	BOC(5,2)
	S(SPS)	2402.028	BPSK(1)
	S(RS)	2492.020	BOC(5,2)

### **2.2 Space Constellation**

NavIC space segment is formed by a constellation of 7 satellites, which will broadcast ranging signal along with navigation message. The satellites will be placed in two different orbital planes, 3 satellites in Geo-Stationary Orbit (GEO) and 4 satellites in Geo-Synchronous Orbit with inclination of 27°. The NavIC constellation having orbit parameters as mention in Table-2. Galileo has 27 MEO satellites and GPS has 24 MEO satellites as mention in Table-3. The constellation parameters of GPS and Galileo are taken as taken in [23-25].



Table 2: Constellation Parameter of IRNSS

Satellite	Longitude	Inclination
Satemie	(deg)	(deg)
1A	55	27±2
1B	55	27±2
1C	83	0
1D	111.75	27±2
1E	111.75	27±2
1F	32.5	0±5
1 <b>G</b>	129.5	0±5

**Table 3: Constellation Parameter GALILEO and GPS** 

Parameter	GALILEO	GPS
Constellation	Wallton 27/2/1	24/6
Parameters	walker 27/3/1	
Eccentricity	0	0
Inclination (deg)	56	55
Somi Majon Aria	20002 707 lim	26559.7
Semi Wajor Axis	29995.707 KIII	km

## 3. COMPUTATION OF INTERFERENCE

Effective Carrier Power to Noise Density Ratio  $(C/N_0)$  indicates effect of interference on Signal to Noise plus Interference Ratio for both coherent and non-coherent outputs. It is directly related to many aspects of receiver performance including Signal acquisition, Data demodulation, Carrier tracking and code tracking. The computation of interference is done as stated in [5].  $(C/N_0)_{\text{eff}}$  is given by equation -1.

$$\left(\frac{C}{N_{0}}\right)_{\text{eff}} = \frac{C}{\sum_{\substack{B_{r}/2\\ N_{0} + \frac{-B_{r}/2}{B_{r}/2}} P_{l}(f)P_{s}(f)df}} \int_{-B_{r}/2}^{B_{r}/2} P_{s}(f)df}$$
(1)

Where C is the received power of desired signal,  $N_0$  is the PSD of Gaussian White Noise,  $C_I$  is received power of interfering signal,  $P_I(f)$  and  $P_s(f)$  are PSD of interfering and desired signal normalized to unit area over infinite limits.  $B_r$  is front end bandwidth of receiver.

In practice, Front End Bandwidth of receiver is not larger than the emission bandwidth of desired signal. The emission Bandwidth of interfering signal is not always equal to that of desired signal. Therefore, we calculate PSDs of desired and interfering signal normalised to unit area over their own emission bandwidth. This is given in [5].

$$P_{s}(f) = \frac{P_{s}'(f)}{\int_{-B_{et}/2}^{B_{et}/2} P_{s}'(f) df}$$
$$P_{l}(f) = \frac{P_{l}'(f)}{\int_{-B_{et}/2}^{B_{et}/2} P_{l}'(f) df}$$
-------(2)

Where  $P_s'(f)$  and  $P_1'(f)$  are the power spectral densities of the desired and interfering signals before normalization,  $B_{es}$  is the emission bandwidth of the desired signal, and  $B_{el}$  is the emission Bandwidth of the interfering signal.

The receiver will face interfering signals from different satellites so the value of  $C/N_0$  becomes [5]

$$\left(\frac{C}{N_0}\right)_{eff} = \frac{C}{N_0 + I_{Intra} + I_{Inter}}$$
(3)

Where  $I_{intra}$  is the equivalent noise PSD of the intrasystem interference including the interfering signals from the satellites belonging to the same system as the desired signal and  $I_{nter}$  is the equivalent noise PSD of the intersystem interference which contains the interfering signals from the counterpart system of the desired signal.

The GNSS receiver is stationary at the earth surface so satellite movement causes frequency diversity, which is called as Doppler Frequency Offset due to Doppler Effect. Thus, the equivalent noise PSD [5] is given by equation (4)

$$I_{Intra} = \frac{\sum_{j=1}^{N_X} C_j \kappa_{js}}{\int\limits_{-B_r/2}^{B_r/2} P_s \left(f + f_{dops}\right) df}$$
(4)

When focusing on the intra system interference, the degradation of C /  $N_0$  caused by the signals

From the same system as the desired signal can be expressed as [5] (equation 5):

$$\left(\frac{C}{N_0}\right)_{\text{deg\_Intra}} = \frac{\frac{C}{N_0}}{\frac{C}{N_0 + I_{Intra}}}$$
$$= 1 + \frac{I_{Intra}}{N_0} \qquad (5)$$

Which can be written in dB as (equation 6)



$$\left(\frac{C}{N_0}\right)_{\text{deg\_Intra}} (\text{dB}) = 10 \cdot \log\left(1 + \frac{I_{\text{Intra}}}{N_0}\right)$$

The degradation of caused by the intersystem interference is given by [5] (equation 7)

$$\left(\frac{C}{N_0}\right)_{\text{deg\_Inter}} = \frac{\frac{C}{N_0 + I_{\text{Intra}}}}{\frac{C}{N_0 + I_{\text{Intra}} + I_{\text{Inter}}}} = 1 + \frac{I_{\text{Inter}}}{N_0 + I_{\text{Inter}}}$$

Which can be expressed in dB as,

$$\left(\frac{C}{N_0}\right)_{\text{deg\_Inter}} \left(\text{dB}\right) = 10 \cdot \log\left(1 + \frac{I_{Inter}}{N_0 + I_{Intra}}\right)$$
(7)

## 4. INTERFERENCE ANALYSIS

The evaluation of the intersystem interference between the NavIC L5 and Galileo E5a signals

as well as the NavIC L5 and GPS L5 signals will be presented in this section. The degradation of the worst case is computed, which means the maximum received power of the interfering signal and the minimum received power of the desired signal are considered. The Satellite Tool Kit (STK) and MATLAB are used for simulation.

The simulations are divided into the following four scenarios:

- 1. Galileo E5a signal is interfered by the NavIC L5 signal
- 2. NavIC L5 signal is interfered by the Galileo E5a signal
- 3. GPS L5 signal is interfered by the NavIC L5 signal
- 4. NavIC L5 signal is interfered by the GPS L5 signal

#### **4.1 Simulation Parameters and results**

The received power changes during different times and different locations. Received power calculated taking into account constellation and dynamic link budget is given by [5].

$$C_j = P_j + G_j - A_{dist} - A_{atm} - A_{pol} + G_{usr}$$

----- (8)

Where  $P_j$  is the emission power at satellite j,  $G_j$  is the satellite antenna gain,  $A_{dist}$  is the attenuation of the signal due to the distance between satellite *j* and user,  $A_{atm}$  is the attenuation of the signal due to atmospheric loss,  $A_{pol}$  is the polarization mismatch loss, and  $G_{usr}$  is the receiver antenna gain.

The expression of calculating  $A_{dist}$  is given by equation 9.

$$A_{dist} = 10 \log_{10} \left( \frac{c}{4\pi df_c} \right) \tag{9}$$

Where c is the speed of light, d is the distance between satellite and user, and fc is the centre

Frequency. The attenuation of the signal due to atmospheric loss  $A_{atm}$  is estimated to be 0.5 dB for all services and systems, the polarization mismatch loss  $A_{pol}$  is assumed to be 1.0 dB, the receiver antenna gain  $G_{usr}$  is set to 0 dBic.

The simulation parameters related to simulation are summarised in Table-4 below:

Parameter	NavIC interferes with GPS	GPS interferes with NavIC	Galileo interferes with NavIC	NavIC interferes with Galileo
Simulation Period	3 days	3 days	3 days	3 days
Elevation Angle	10 deg	10 deg	10 deg	10 deg
Emission Power (dBW)	NavIC:36.8 GPS:16.14 1	NavIC:35.8 GPS:18.973	Galileo:15. 68 NavIC:35.8	NavIC:36. 8 Galileo:14 .232
Emission Bandwidth (MHz)	NavIC:24 GPS:30.69	NavIC:24 GPS:30.69	Galileo:90 NavIC:24	Galileo:90 NavIC:24
Front End Bandwidth (MHz)	24.552	24.552	24.552	24.552

The antenna type has been assumed to be Parabolic and the modulation to be BPSK for all cases. The mean received power for maximum emission power of interfering signal and minimum emission power of derived signal of the systems are shown in figure 1-4.

Figure 5 shows the results of intersystem interference when NavIC is interfered by Galileo. Figure 6 shows the results of intersystem interference when Galileo is interfered by NavIC.

Figure 7 shows the results of intersystem interference when NavIC is interfered by GPS.

Figure 8 shows the results of intersystem interference when GPS is interfered by NavIC.

Mean interference in the case when Galileo is interfered by NavIC, is almost 1.1dBHz more than in case when NavIC is interfered by Galileo. Similarly, when GPS is interfered by NavIC, mean interference is almost 1.05dBHz more than in case when NavIC is interfered by GPS.





Figure 1: Mean Received Power when NavIC is interfered by Galileo



Figure 2: Mean Received Power when Galileo is interfered by NavIC



Figure 3: Mean Received Power when NavIC is interfered by GPS



Figure 4: Mean Received Power when GPS is interfered by NavIC



Figure 5: Maximum Interference on NavIC due to Galileo Min: 50dBHz and Max: 51.2dBHz



Figure 6: Maximum Interference on Galileo due to NavIC Min: 51dBHz and Max: 52.4dBHz



Figure 7: Maximum Interference on NavIC due to GPS Min: 50.1dBHz and Max: 50.9dBHz



Figure 8: Maximum Interference on GPS due to NavIC Min: 51dBHz and Max: 51.9dBHz



## 5. CONCLUSION

This paper analyses compatibility of NavIC with GPS and Galileo respectively over Indian region. The worst case analysis has been carried out which means intersystem interference will not be larger than the results presented in the paper under the given assumptions. These simulations ensure compatibility between navigation systems. From the simulations, we can conclude that intersystem interference of Galileo due to NavIC is slightly larger than intersystem interference of GAI due to Galileo in Indian region. Similarly, intersystem interference of GPS due to NavIC is slightly larger than intersystem interference of Intersystem interference of NavIC due to GPS in Indian region.

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